

PRE LOAD

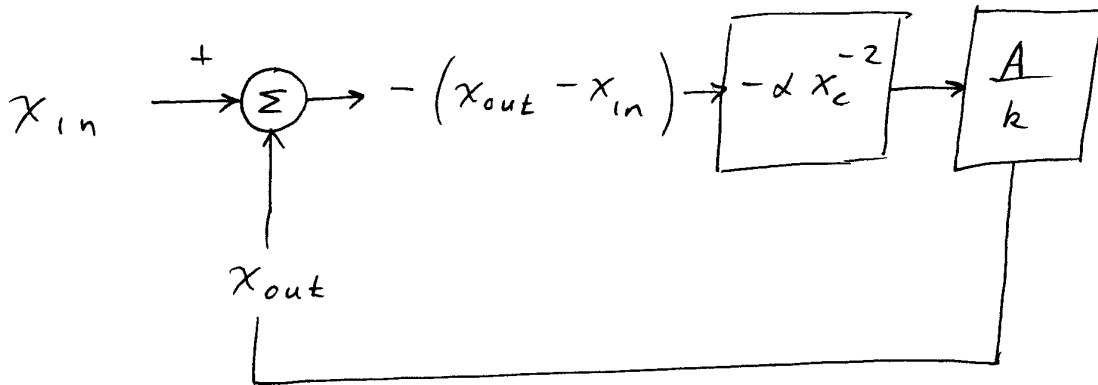
$$F = F_0 + k x_{out}$$

$$x_c = \frac{1}{k} (F - F_0)$$

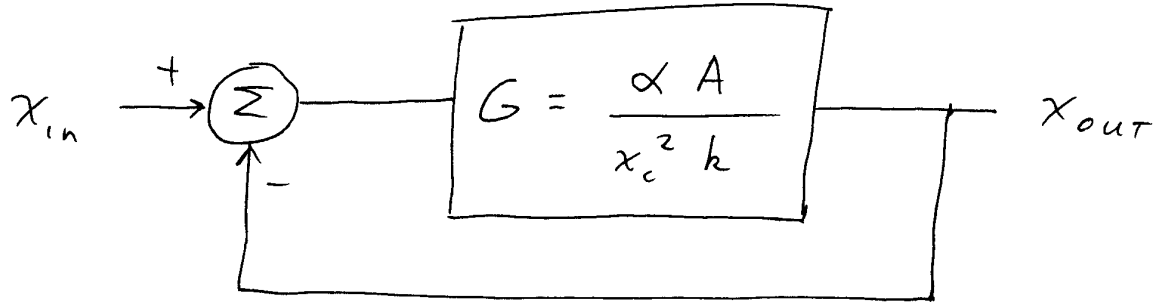
↖ LARGE FOR SOFT
SPRING

NEGATIVE
FEEDBACK LOOP

A: BEARING
AREA



SIMPLIFIED FEEDBACK LOOP

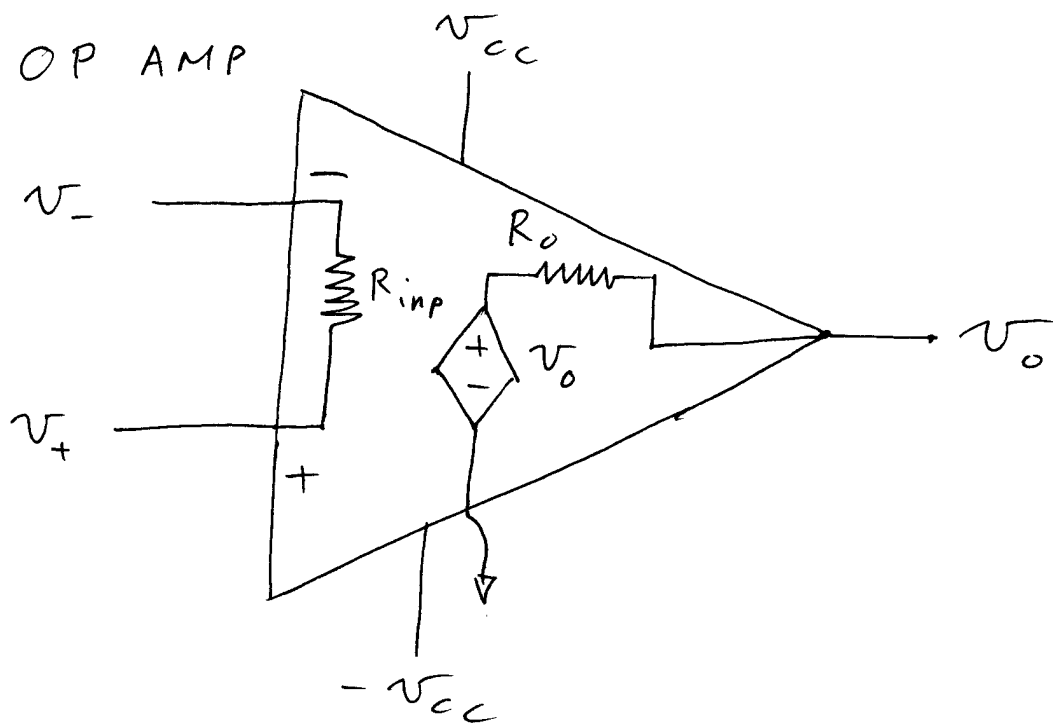


$$x_{out} = G (x_{in} - x_{out})$$

G LARGE, VARIABLE

$$x_{out} = \frac{G}{1+G} x_{in} \approx x_{in}$$

FOR BIG G



IDEAL OP AMP

$$v_o = G (v_+ - v_-) \quad G \rightarrow \infty$$

$$R_i \rightarrow \infty \quad R_o \rightarrow 0$$

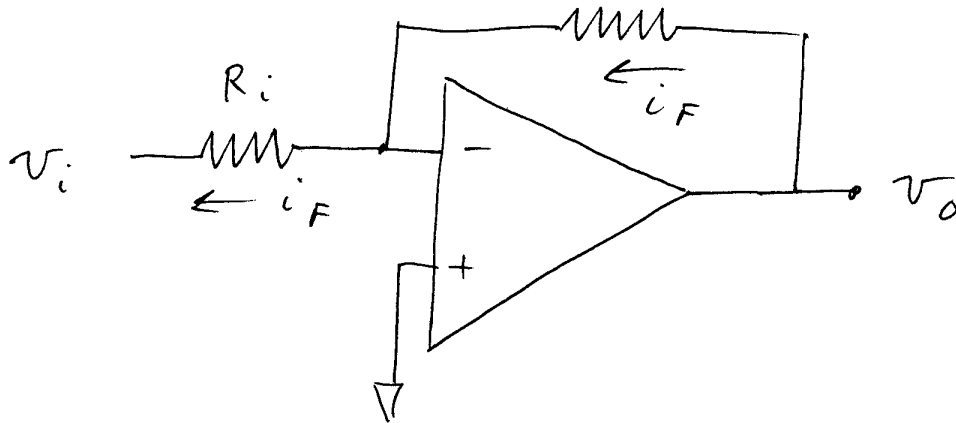
SATURATION

$$-V_{cc} < v_o < V_{cc}$$

V_{cc} TYPICALLY 10-15 Volts

OUR FIRST OP-AMP CIRCUIT

INVERTING AMP R_F



ASSUME $R_{inp} \rightarrow \infty$ (NO CURRENT IN OR OUT OF - OR + INPUTS)

$$v_+ = 0 \quad i_F = \frac{v_o - v_i}{R_i + R_F}$$

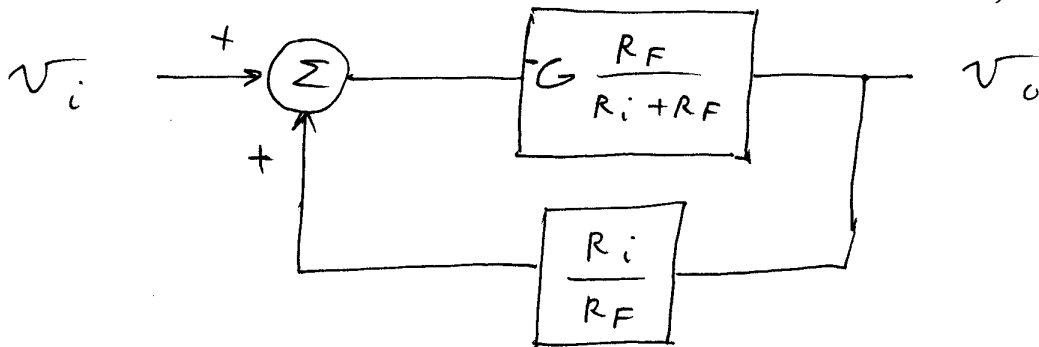
$$v_- = v_i + i_F R_i$$

$$= v_i + \left(\frac{R_i}{R_i + R_F} \right) (v_o - v_i)$$

$$v_o = G (v_+ - v_-)$$
$$= G \left(-v_i + \left(\frac{R_i}{R_i + R_F} \right) (v_o - v_i) \right)$$

$$v_o = -G \left(\frac{R_i}{R_i + R_F} v_o + \frac{R_F}{R_i + R_F} v_i \right)$$

$$= -G \frac{R_F}{R_i + R_F} \left(\frac{R_i}{R_F} v_o + v_i \right)$$



$$v_o = -G' \left(v_i + \frac{1}{\beta} v_o \right)$$

$$G' = G \frac{R_F}{R_i + R_F} \quad \beta = \frac{R_F}{R_i}$$

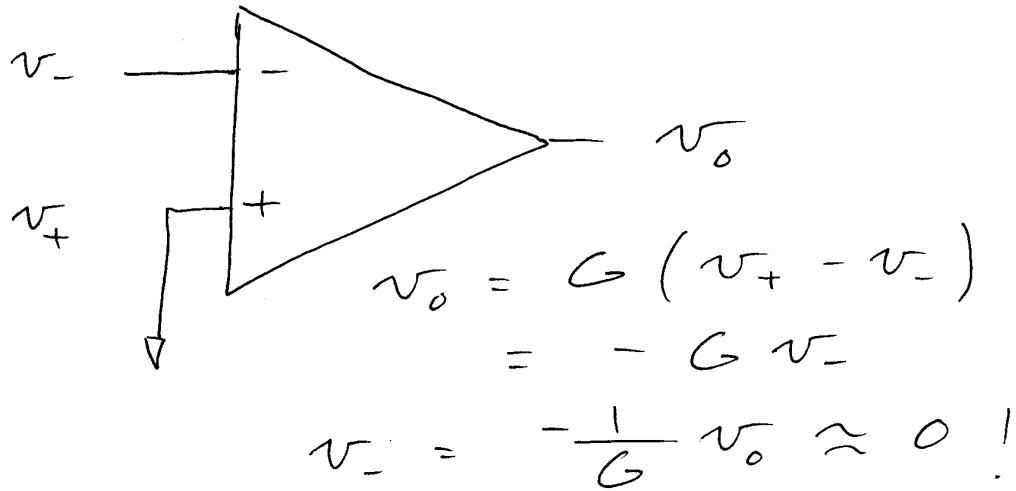
$$v_o = \frac{-G'}{1 + \frac{G'}{\beta}} v_i$$

$$= \frac{1}{\frac{1}{G'} + \frac{1}{\beta}} v_i = \frac{-1}{\frac{1}{\beta}} v_i$$

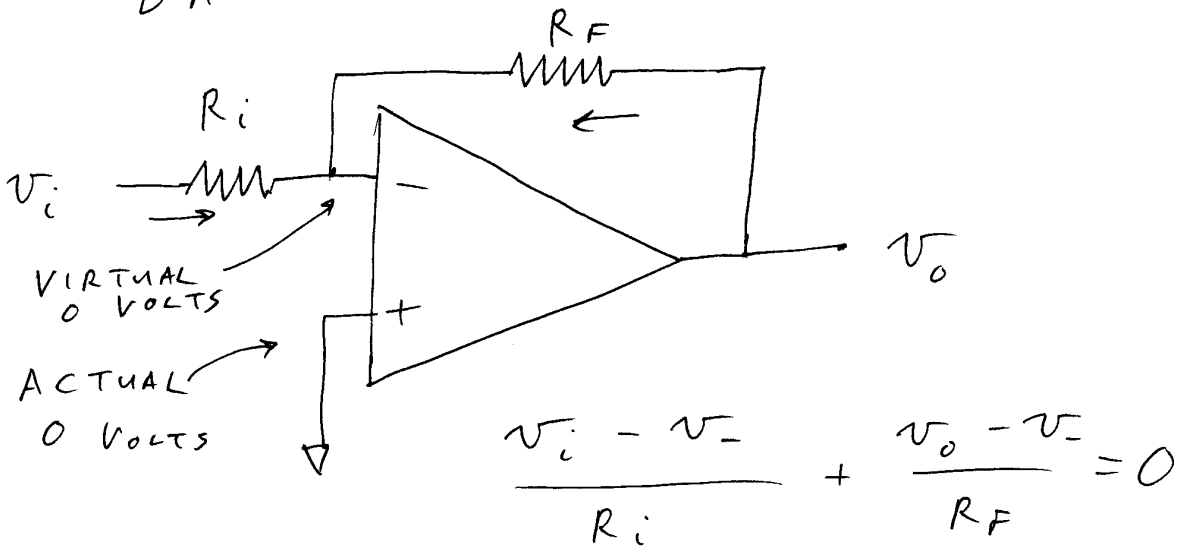
$$= -\beta v_i$$

$$\text{As } G' \rightarrow \infty \quad \frac{1}{G'} \rightarrow 0$$

VIRTUAL REFERENCE VOLTAGE



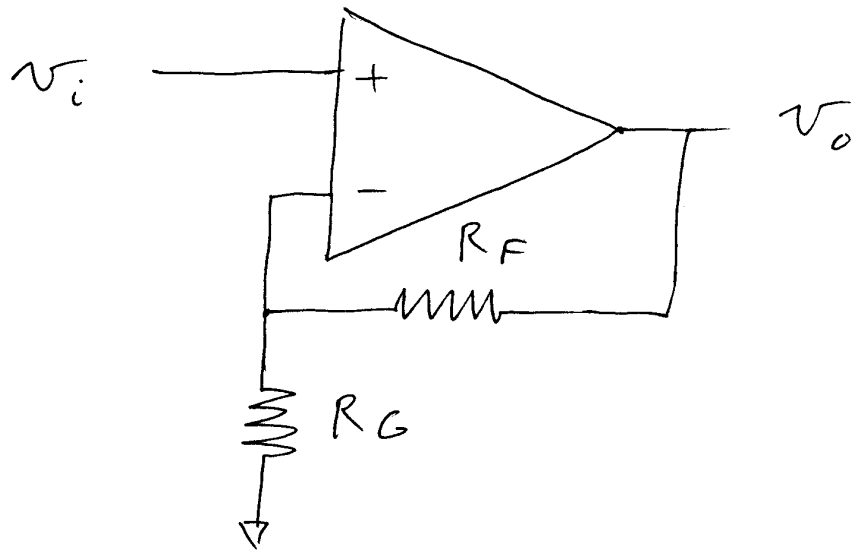
BACKWARDS NODE EQ



$$v_- = v_+ = 0$$

$$v_o = -\frac{R_F}{R_i} v_i$$

NON-INVERTING OP AMP



VOLTAGE DIVIDER

$$v_- = \frac{R_G}{R_G + R_F} v_o$$

VIRTUAL REFERENCE VOLTAGE

$$v_- = v_+ = v_i$$

$$v_i = \frac{R_G}{R_G + R_F} v_o$$

$$v_o = \frac{R_G + R_F}{R_G} v_i = \left(1 + \frac{R_F}{R_G}\right) v_i$$